

Amendments to the Specification

Please amend paragraph [0029] as follows:

[0029] For ease of reference, reference numerals in the accompanying drawings typically are in the form “drawing number” followed by two digits, xx; for example, reference numerals on Figure 4 may be numbered 4xx; on Figure 5, reference numerals may be numbered 5xx, and so on. In certain cases, a reference numeral may be introduced on one drawing and the same reference numeral (with a different drawing number indicator) may be utilized on other drawings to refer to the same item. For example, the following reference numbers are used:

<u>Reference Numbers</u>	<u>Element</u>
<u>405, 505</u>	<u>switching valve</u>
<u>106, 406, 506, 606, 706</u>	<u>chemical source (or process gas)</u>
<u>407, 507</u>	<u>switching valve</u>
<u>108, 408, 508, 608, 708</u>	<u>chemical source (or process gas)</u>
<u>409, 509</u>	<u>pressure controller</u>
<u>110, 410, 510, 610, 710, 810</u>	<u>chamber or reactor</u>
<u>411, 511</u>	<u>pressure controller</u>
<u>112, 412, 512, 612, 712, 812</u>	<u>heater assembly</u>
<u>114, 414, 514, 614, 714, 814</u>	<u>wafer</u>
<u>116, 416, 516, 616, 716</u>	<u>shut-off valve</u>
<u>117, 417, 517, 617, 717</u>	<u>controller</u>
<u>118, 418, 518, 618, 718</u>	<u>shut-off valve</u>
<u>119, 419, 519, 619, 719</u>	<u>controller</u>
<u>120, 420, 520, 620, 720</u>	<u>throttle valve</u>
<u>122, 422, 622, 722</u>	<u>feedback control system</u>
<u>124, 424, 524, 624, 724, 824</u>	<u>reactor purge pathway</u>
<u>126, 426, 526, 626, 726, 826</u>	<u>reactor purge pathway</u>
<u>128, 428, 528, 628, 728, 828</u>	<u>input or entrance to chamber</u>
<u>130, 430, 530, 630, 730, 830</u>	<u>pump</u>
<u>432, 532</u>	<u>pump</u>
<u>434, 534</u>	<u>valve</u>

Please amend paragraph [0051] as follows:

[0051] To achieve the multi-level purge methods described above, an ALD apparatus 400 having a second purge conduit that is introduced upstream of the chemical gas switching manifold and in parallel with the first purge conduit is provided. This arrangement (which may be termed a dual flow purge manifold 403) is illustrated in **Figure 4**. Both purge sources may be pressure controlled (e.g., using pressure controllers 409 and 411) with set points of pressure that can be widely different. Given the current state of the art, the pressure controllers 409 and 411 cannot be fast gas switched below several hundred milliseconds (however, future pressure controllers may allow for direct, fast electronic control). We avoid this shortcoming by passing the pressurized gas through fast switching pneumatic valves (with conductances determined by the conduit lines, elbows, valve and any restrictor components in the lines between the pressure ~~sources~~ controllers 409/411 down to and including the entrance 428 to the reactor 410). This implementation has each purge conduit leading to switching valves 405 and 407. These valves may be as fast (e.g., on the order of 20 msec) as are used for precursor injection valves 416 and 418.

Please amend paragraph [0064] as follows:

[0064] The reactor pressure for a reactor of very large conductance (compared with the conductances in line from ~~source~~ controller 642) placed in series between an upstream flow limiting conductance and downstream flow limiting conductance can be approximated by an expression for the chamber pressure:

$$P_{\text{cham}} \sim {}^uP \times [(1/{}^dC) / (1/{}^dC + 1/{}^uC)] \quad (1),$$

where uP is the upstream pressure that may be set with a pressure controller, and dC and uC are the downstream and upstream conductances, respectively. The reciprocal conductances are proportional to the flow impedance, so at any constant flow the chamber pressure is just the ratio of pressure drop across the downstream impedance to the total impedance.